

# **New theoretical approach describing the pressure effect on the melting temperature**

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# HISTORY

- The effect of pressure on the melting temperature was detected by Perkinson in 1826. Compressing acetic acid [ $\text{CH}_3\text{COOH}$ ] to 1100 Atm. he found that the substance became crystallized.
- Ever since then numerous effort has been made to describe the effect of pressure on the melting temperature. The current standing of the research is outlined here.

# THEORETICAL DESCRIPTIONS

- Clapyeron describes the  $dp/dT$  slope of co-existing gas-liquid phase in 1834
- Clausius extends to liquid-solid phase in 1850, which is know as the Clausius-Clapyeron relationship

$$\frac{dp}{dT} = \frac{\Delta H_f}{T\Delta V} = \frac{\Delta S}{\Delta V}$$

- The Lindemann melting formula (1910) is

$$T_m = cMa^2\theta_D^2$$

$$a = \sqrt[3]{\frac{V_{\text{mol}}}{N_A}}$$

$$T_m = cV_m^{\frac{2}{3}}\theta_D^2$$

Primarily is used for atmospheric pressure because it is difficult to determine  $V_m$  and  $\theta_D$  at high pressure and temperature.

- Simon and Glatzel (1929) proposed the formula:

$$\frac{p_m - p_o}{a} = \left( \frac{T_m}{T_o} \right)^c - 1$$

Successfully describes the p-T<sub>m</sub> curves of many substances.

Kennedy (1965) shown that the equation does not give satisfactory melting temperature when extrapolated to core pressure

- Kraut-Kennedy (1965)

$$T_m = T_m^o \left( 1 + C \frac{\Delta V}{V_o} \right)$$

$\Delta V/V_o$  is the isothermal dilation

They claimed that in case of iron the linear relationship is valid up to compression of 0.5

- Gilvarry (1965); Vaidya and Gopal (1965)

Using the Lindemann melting criteria it has been shown that

$$C = 2\left(\gamma - \frac{1}{3}\right)$$

- Libby (1966); Mukherjee (1966)

Assuming constant bulk modulus the Kraut-Kennedy relationship can be derived from the Clausius-Clapeyron relationship

$$T_m - T_m^0 = \frac{\Delta V_m}{T_m \Delta S_m} T_m^0 K_0 \frac{\Delta V}{V_0}$$

- Wang (1999) proposed a model and introduced a critical temperature which is equivalent with the melting temperature

Using the EoS and conventional thermodynamic relationships the critical volume relating to the critical temperature is calculated

Deducting the thermal pressure from the actual pressure gives the pressure relating to the melting temperature

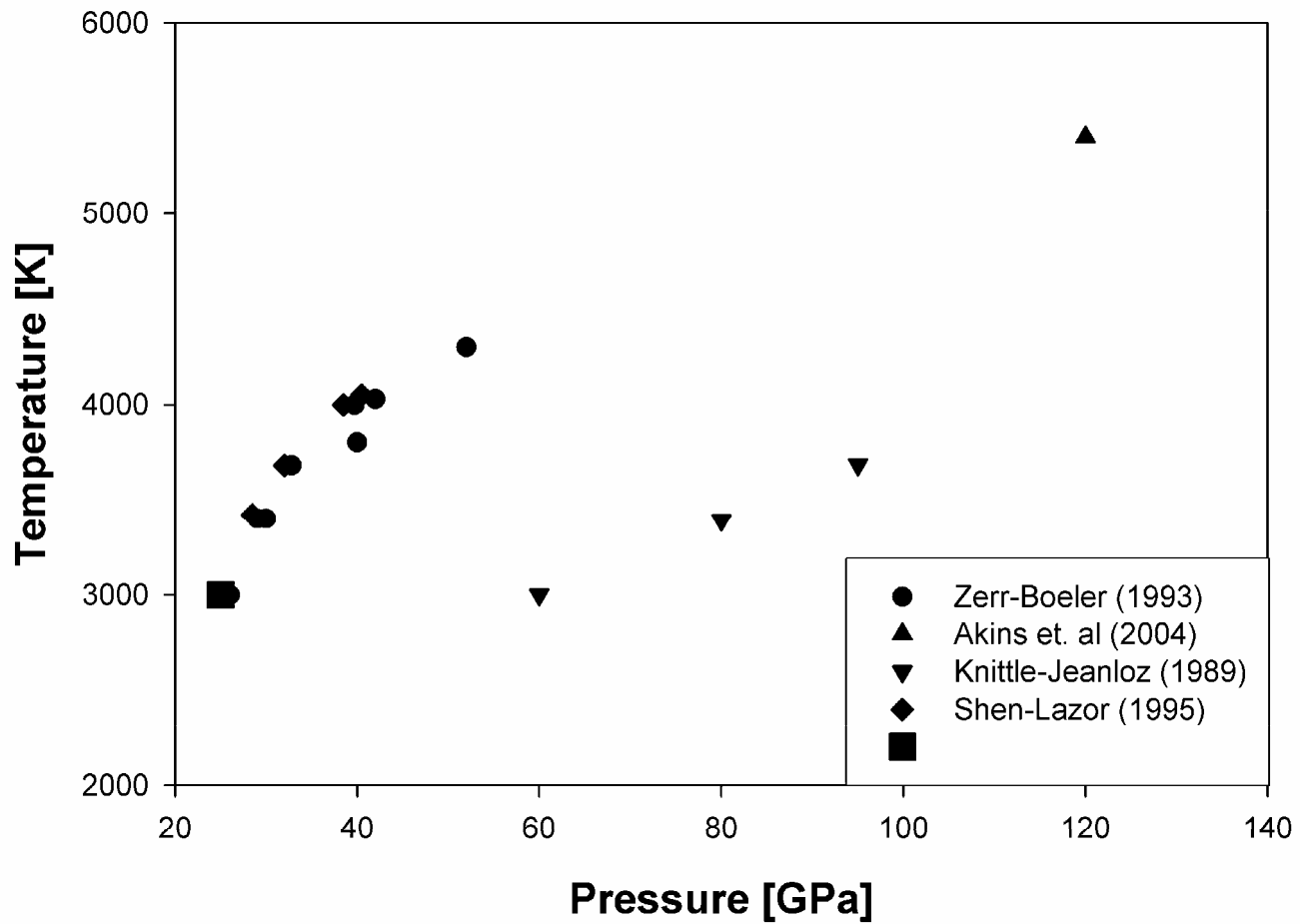
In all of the “theoretical” models the derived formulas contain a “fitting” parameter with no physical meaning.

The descriptions therefore are semi empirical.

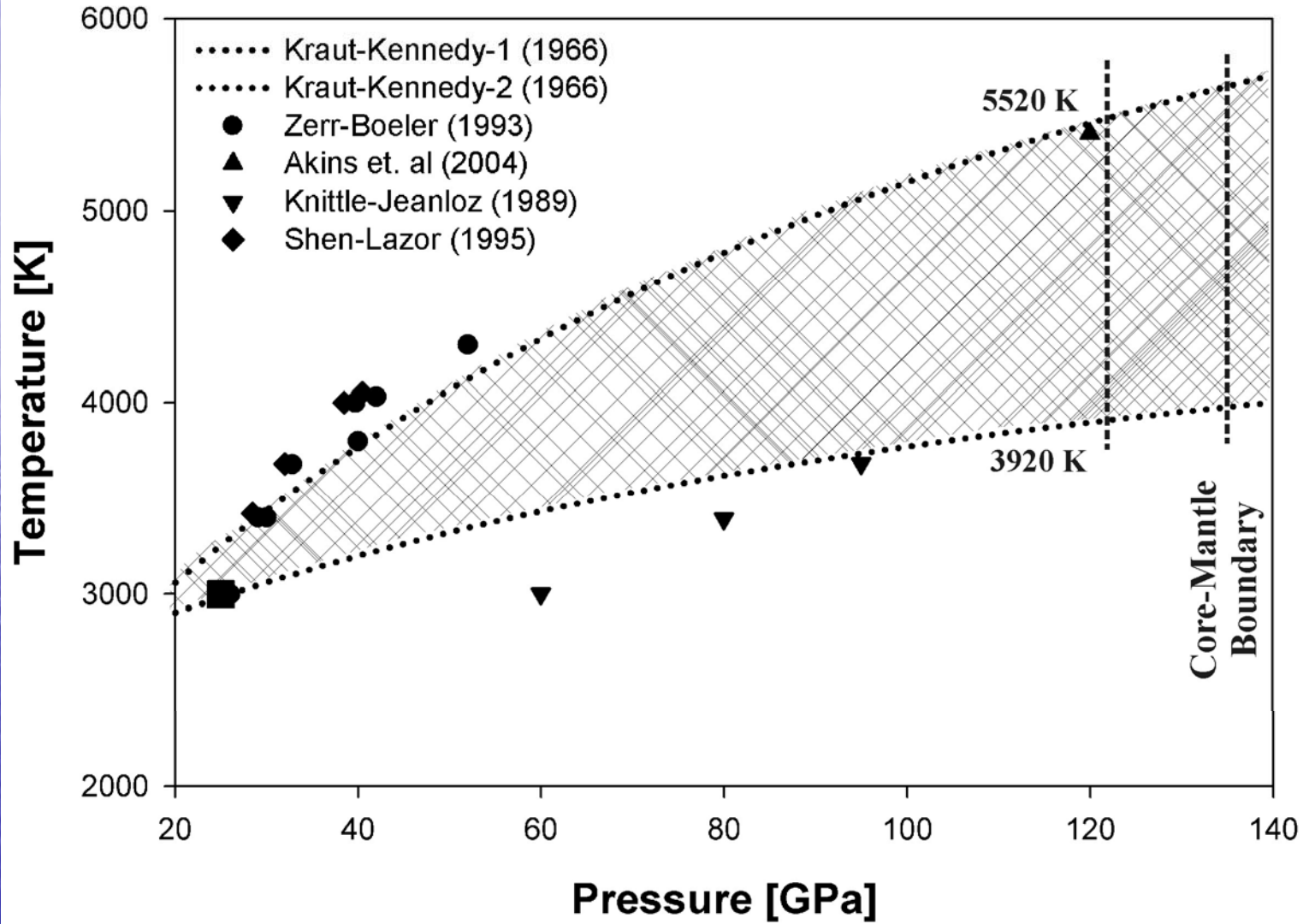
The uncertainties in the theoretical descriptions can be complemented by experiments.

Let's do experiments!

# Perovskite



# Perovskite



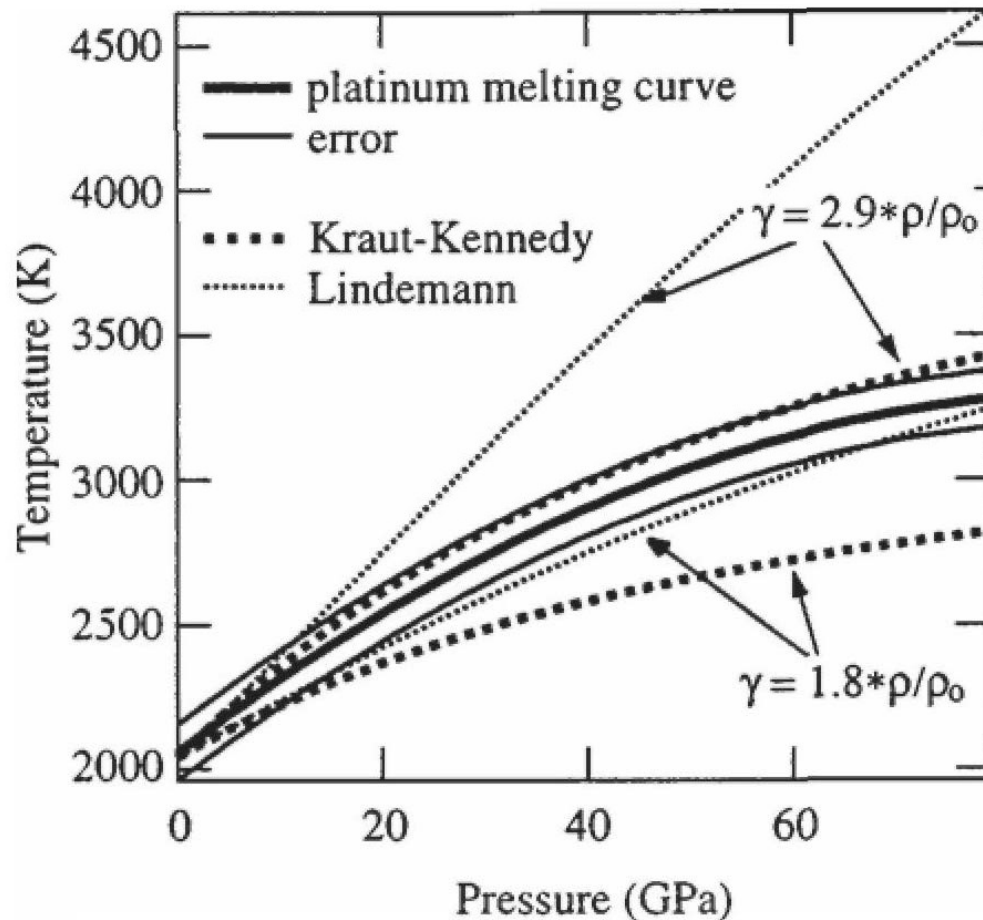


FIG. 6. Comparison of the melting curve determined here (bold solid line with solid line error envelope) with melting curves calculated using the Lindemann (narrow dotted line) and Kraut-Kennedy (bold dotted line) equations. Two curves for each are shown and are bounded by the experimentally determined range of values for the Grüneisen parameter, 1.8–2.9.

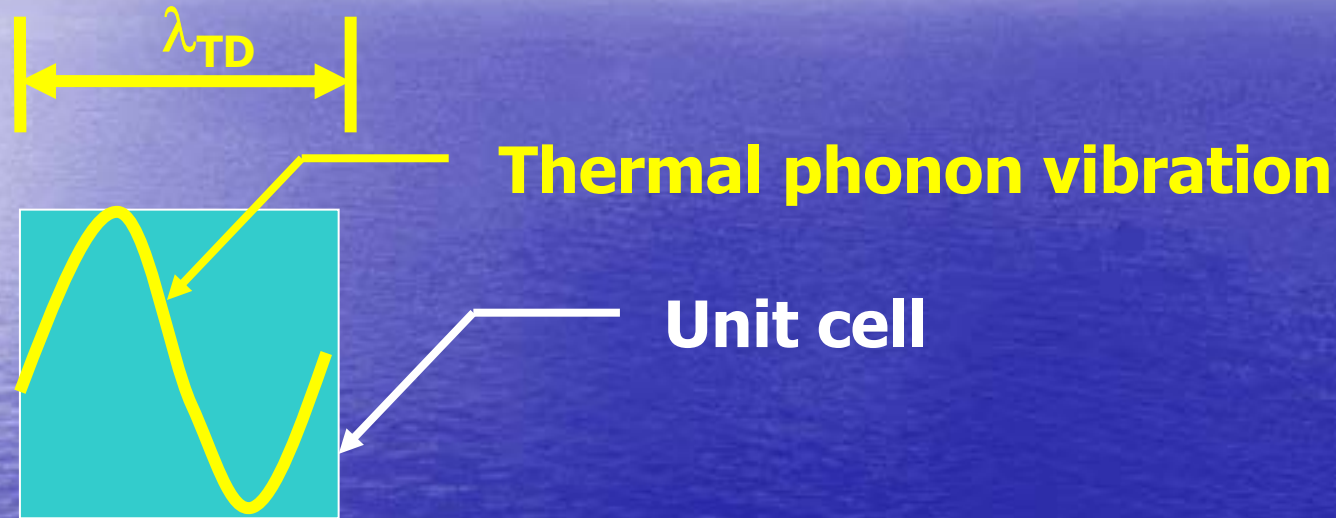


**There is a need for a  
reliable theoretical model.**



# **Background of the proposed model**

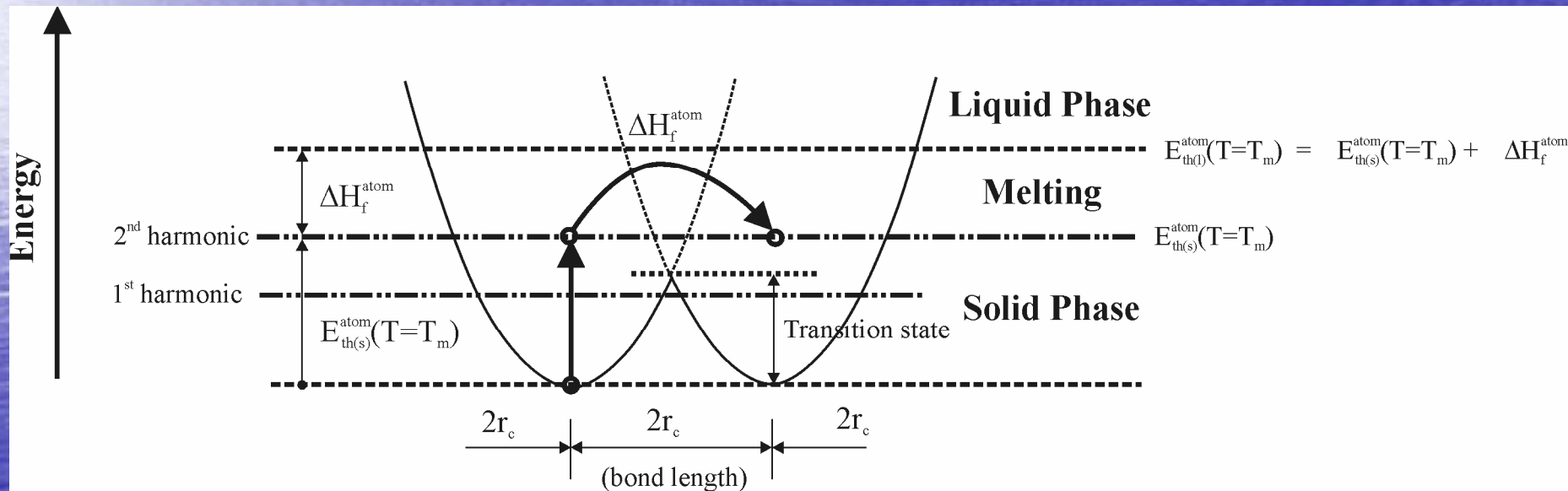
# Physical explanation of the Debye temperature

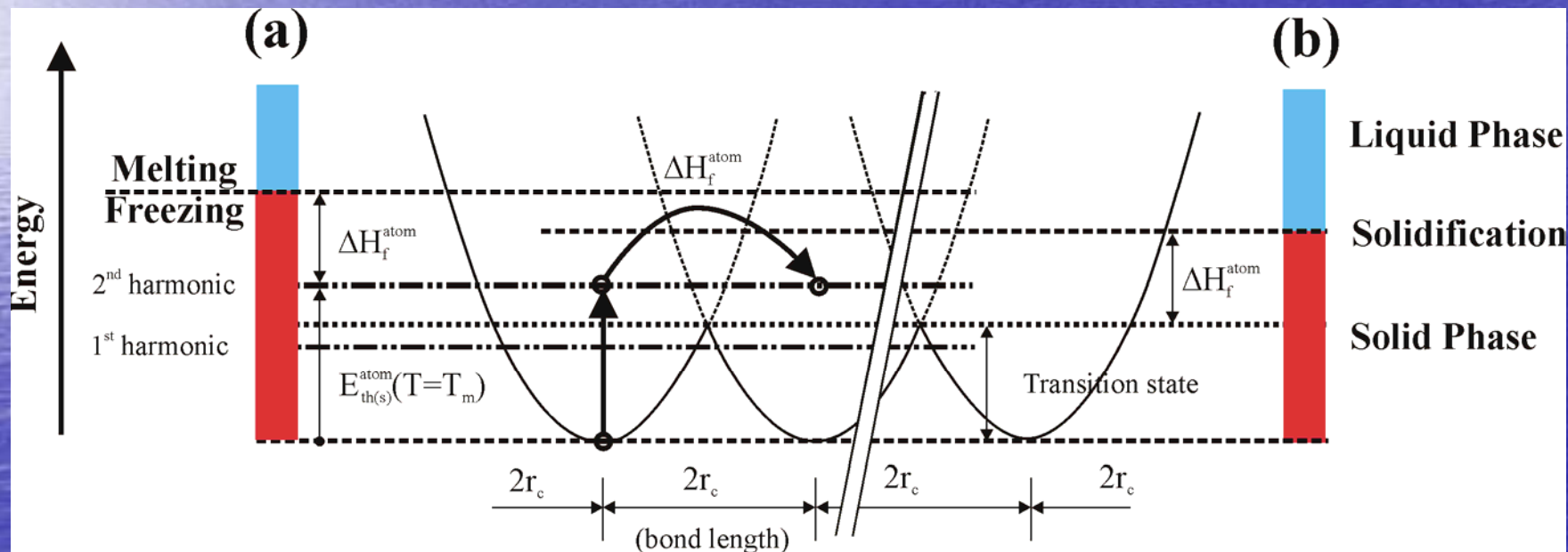


$$T_D \longrightarrow \lambda_{TD} = a$$

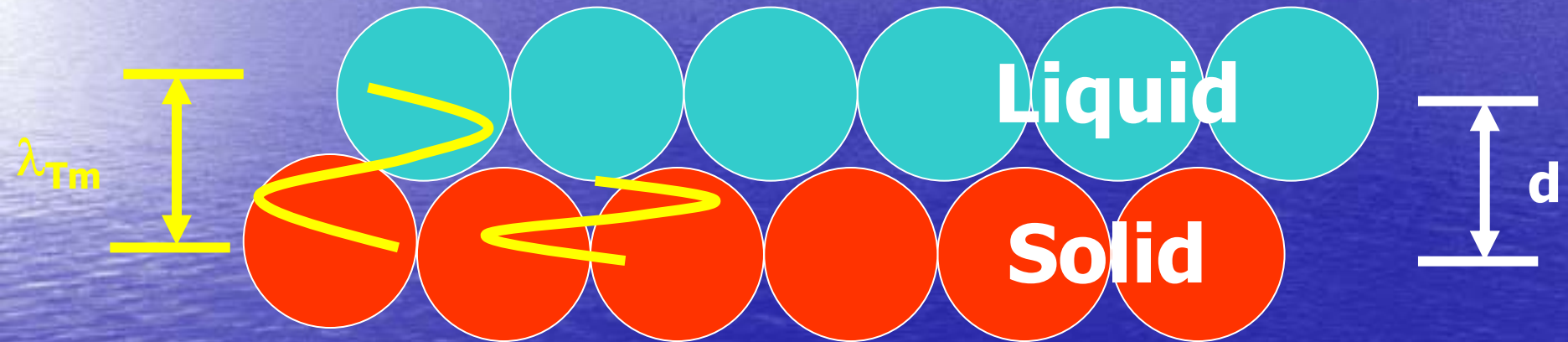
Element	Crystal Structure	Transverse Sound Velocity [ $\times 10^3 \text{ ms}^{-1}$ ]	Longitudinal Sound Velocity [ $\times 10^3 \text{ ms}^{-1}$ ]	Mean Sound Velocity [ $\times 10^3 \text{ ms}^{-1}$ ]	Debye Temperature [K]	Unit cell [ $\text{\AA}$ ]	Wavelength of the cut off frequency [ $\text{\AA}$ ]	Difference [%]
Ag	fcc	3.60	1.59	1.79	215	4.09 <sup>a</sup>	4.01	2.1
Al	fcc	6.26	3.08	3.46	394	4.05 <sup>a</sup>	4.21	4.0
Au	fcc	3.24	1.20	1.36	170	4.08 <sup>a</sup>	3.84	5.7
Cu	fcc	4.70	2.26	2.54	315	3.61 <sup>a</sup>	3.87	7.2
Ni	fcc	5.63	2.96	3.31	375	3.52 <sup>a</sup>	4.24	20.3
Pb	fcc	2.16	0.70	0.80	88	4.05 <sup>a</sup>	4.34	7.3
Pt	fcc	3.96	1.67	1.89	230	3.92 <sup>a</sup>	3.94	0.5
Be	hcp	12.55	8.83	9.58	1031	3.58 <sup>c</sup>	4.46	24.5
Mg	hcp	5.78	3.05	3.41	330	5.19 <sup>c</sup>	4.96	4.5
Ti	hcp	6.33	3.11	3.49	380	4.68 <sup>c</sup>	4.41	5.8
Zn	hcp	4.17	2.41	2.68	234	3.82 <sup>c</sup>	5.49	43.6

# Physical explanation of melting





$$T_m \longrightarrow n\lambda_{Tm} = d$$



$T_D$



$\lambda_D$



$a$

$T_m$



$\lambda_{Tm}$



$d$



pressure

$$a/d = \text{const}$$

$$\lambda_D/\lambda_{T_m} = \text{const}$$

$$T_D/T_m = \text{const}$$



$$T_m = c T_D$$

# Calculation

$$T_D = \frac{h}{k_B} \left[ \frac{3n_A}{4\pi} \left( \frac{N_A \rho}{M} \right) \right]^{\frac{1}{3}} V_B = 251.2 (V_{Tm})^{-\left(\frac{1}{3}\right)} V_{B(Tm)}$$

$$V = nV_o^m e^{\frac{-p}{ap+bp^2+K_o} + (\alpha_o + cp+dp^2)T + \left(1 + \frac{cp+dp^2}{\alpha_o}\right)^f gT^2}$$

$$V_{B(Tm)} = \sqrt{\frac{V_{Tm} K_{Tm} (p)}{M_{mol}}}$$

$$p = \frac{3K_{0T}}{2} \left[ \left( \frac{V_{0T}}{V} \right)^{\frac{7}{3}} - \left( \frac{V_{0T}}{V} \right)^{\frac{5}{3}} \right] \left\{ 1 + \frac{3}{4} (K'_0 - 4) \left[ \left( \frac{V_{0T}}{V} \right)^{\frac{2}{3}} - 1 \right] \right\}$$

$$V_{0T} = V_o e^{(\alpha_o + \alpha_1 T)T}$$

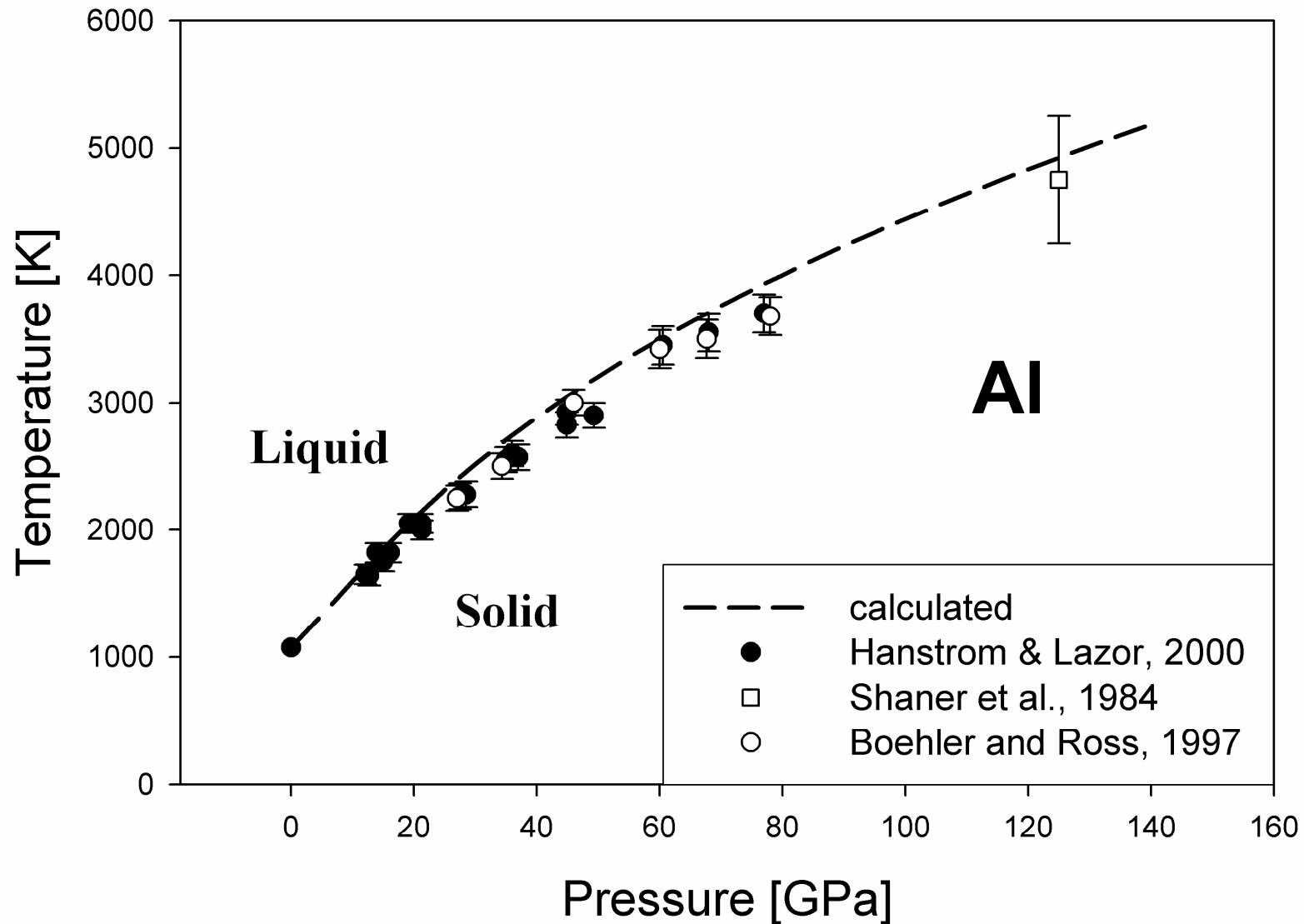
$$K_{0T} = K_o e^{-\int_{T=0}^{T=T} \alpha(T) \delta dT} \cong K_o e^{-(\alpha_o + \alpha_1 T)\delta T}$$

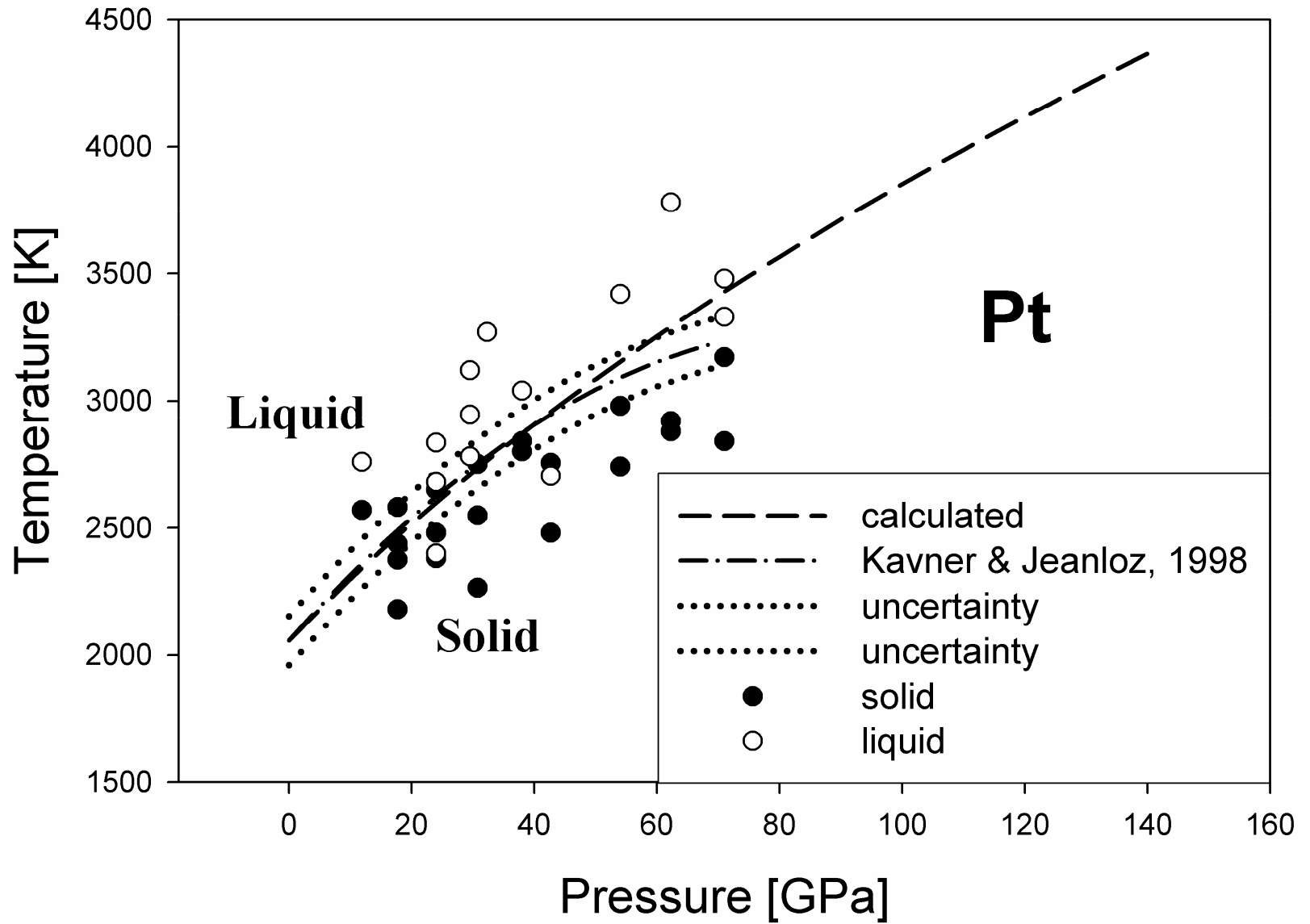
$$K_{p,T} = K_o e^{-(\alpha_o + \alpha_1 T)\delta T} + K'_o p$$

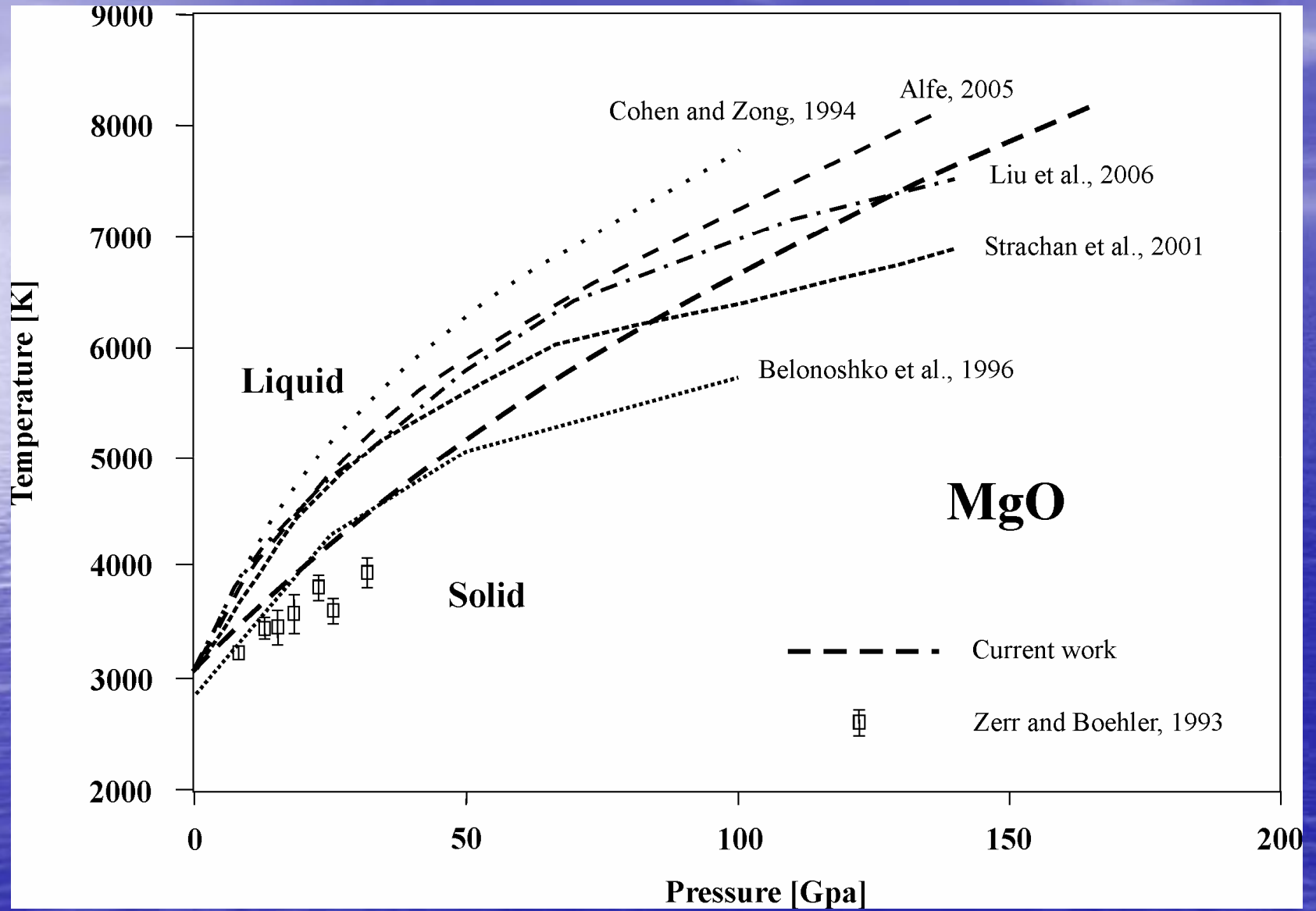
ThermalVolume	$V_o$ [cm <sup>3</sup> ]	$K_o$ [GPa]	$\alpha_o$ [ $\times 10^{-5} \text{ K}^{-1}$ ]	a	b [ $\times 10^{-3}$ ]	c [ $\times 10^{-7}$ ]	d [ $\times 10^{-10}$ ]	g [ $\times 10^{-9}$ ]	f
Al	9.804	100.00	1.184	1.983	-3.145	-0.820	0	10.24	44.5
Pt	9.041	282.42	1.554	2.234	-3.375	-0.283	0	8.631	38.2
MgO	11.149	164.95	2.737	1.717	-2.126	-1.502	2.00	7.901	12.0
MgSiO <sub>3</sub>	24.287	272.5	1.96	1.384	1.430	-1.08	0	0.614	1.0
$\epsilon\text{Fe}$	6.701	171.05	4.029	1.847	-1.276	-0.621	0	-5.087	0.49

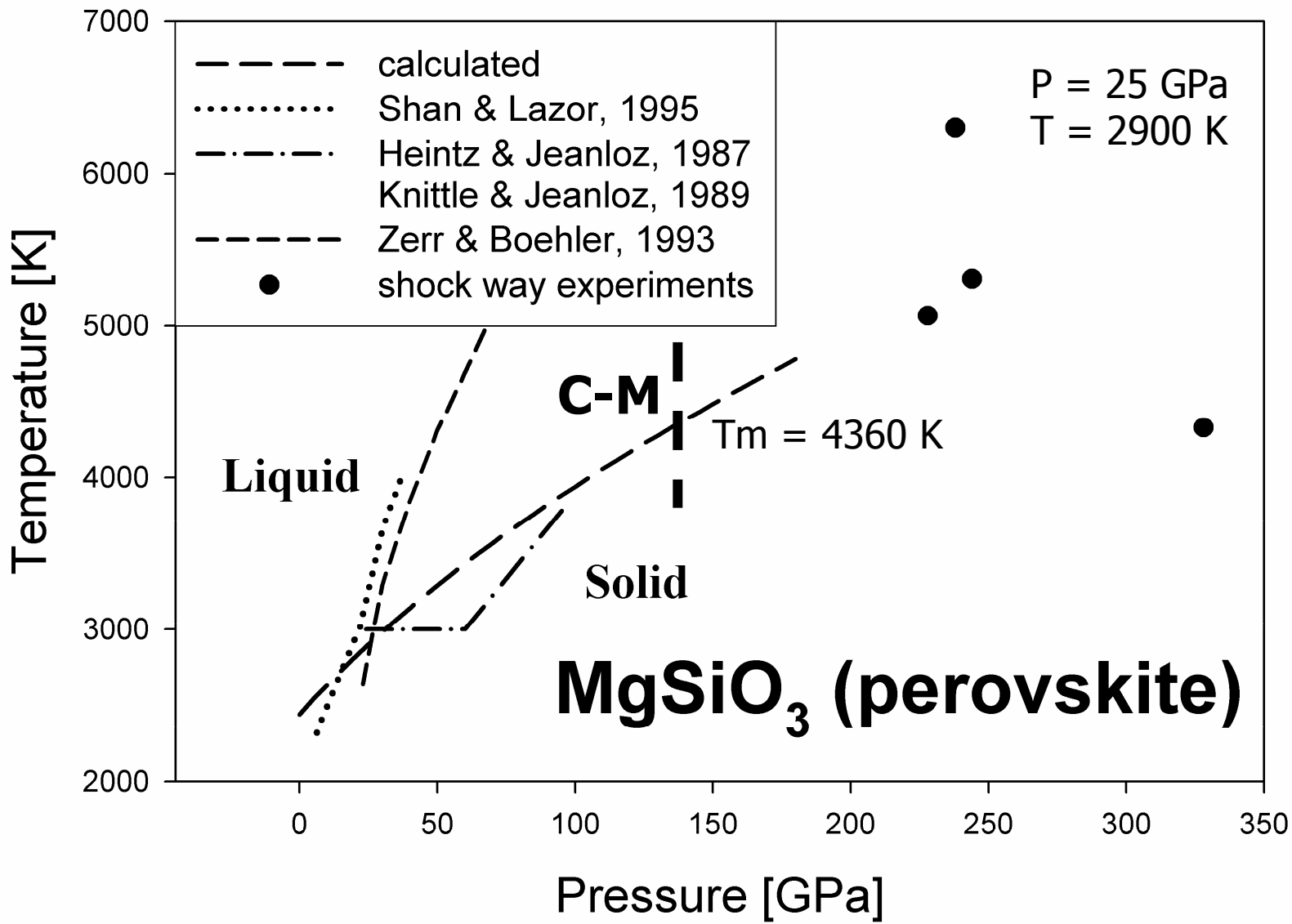
Bulk Modulus	$K_0$ [GPa]	$K_0'$	$\alpha_0$ $\times 10^{-5}$	$\alpha_1$ $\times 10^{-9}$	$\delta$
Al	91.00	3.70	7.650	37.657	12.39
Pt	254.65	6.030	1.750	5.520	4.737
MgO	154.70	4.212	3.317	6.705	3.549
MgSiO <sub>3</sub>	206.79	4.160	2.591	-0.802	3.149
$\epsilon$ Fe	155.41	5.577	5.577	0	2.623

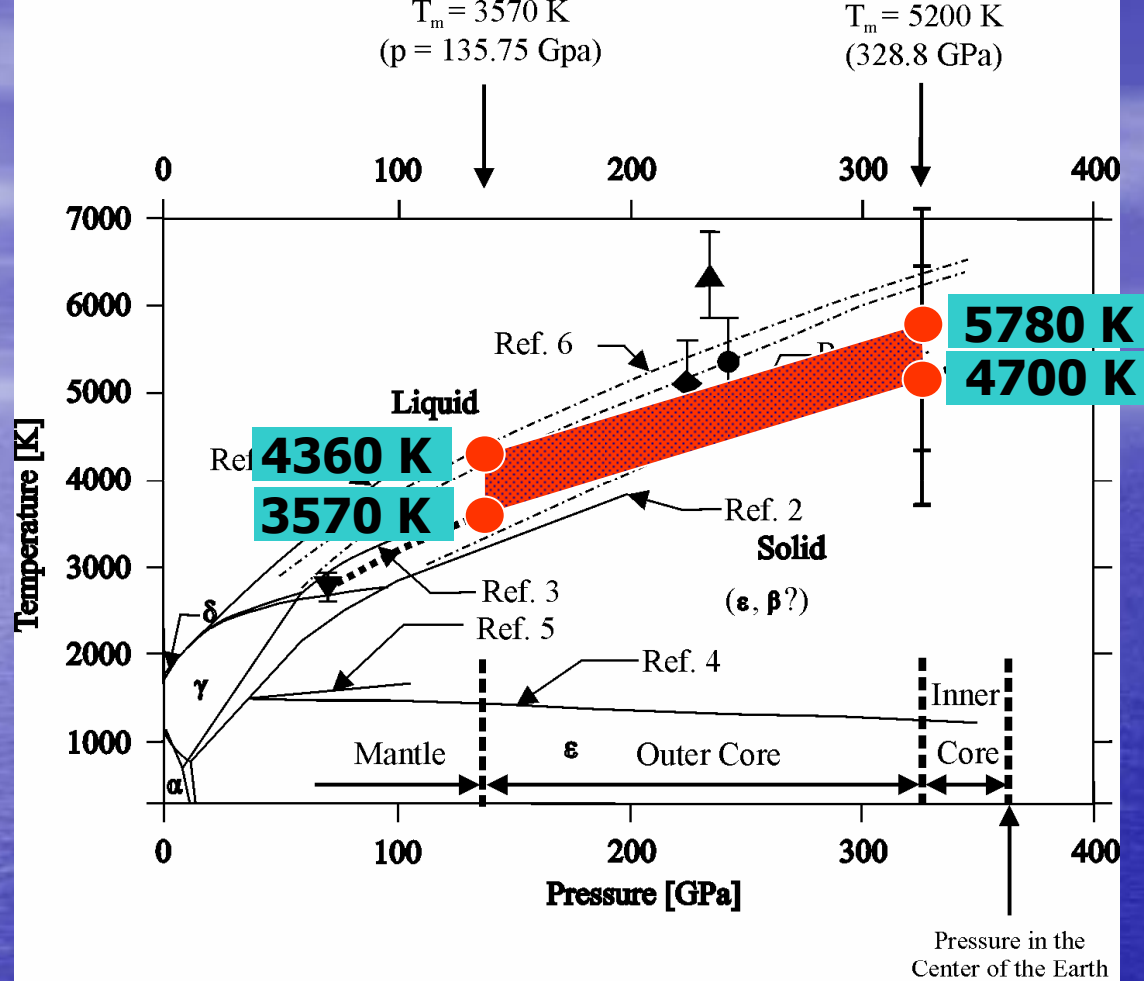
# Results











Solid lines DAC experiments, dashed curves are calculated.

- 1 Williems et al. (1987)
- 2 Boehler (1993)
- 3 Shen et al. (1998)
- 4 Saxena-Dubrovinsky (2000)
- 5 Andraut et al. (2000)
- 6 Alfe et al. (2002)
- 7 Laio et al. (2000)
- Triangle Yoo et al. (1995)
- Circle Brown-McQueen (1986)
- Reverse Triangle Ahrens et al. (2002)
- Diamond Nguyen-Holmes (2005)
- Open circles temperature from EoS

$P = 72 \text{ GPa}$

$T = 2800 \text{ K}$

# Conclusions

- First principle theoretical description of the pressure-melting temperature relationship is proposed.
- Assuming that the ratio of the thermal phonon wavelength at the melting and Debye temperature is constant and using the conventional thermodynamic relationships, equation describing the pressure effect on the melting temperature, is derived.
- The equation is tested against the experiments of Al, Pt, MgO, MgSiO<sub>3</sub> and epsilon Fe with positive results.
- If the boundary conditions are known and the EoS of the substance is available then the p-T<sub>m</sub> curve can be calculated.
- From the melting temperatures and EoSs the proposed constrains on the geotherm are:  
CMB: 3570-4360 K            and            ICB: 4700-5780 K.

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